

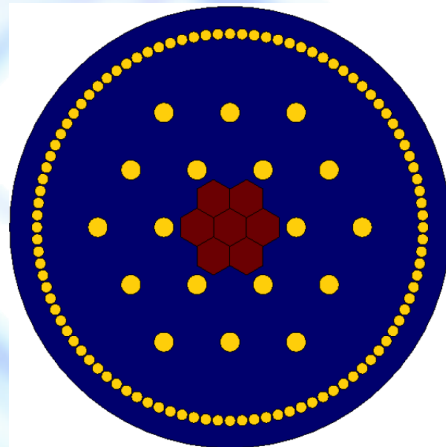
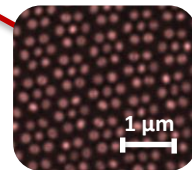
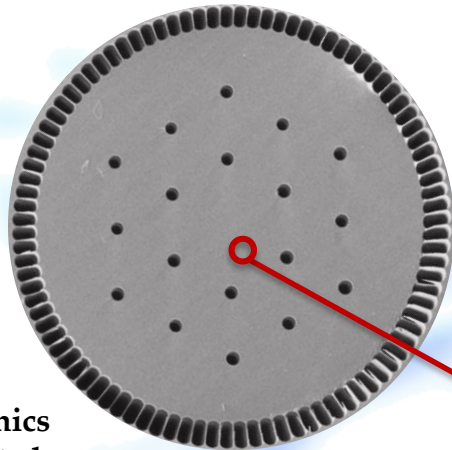
LMA ACTIVE FIBRE FOR HIGH POWER LASERS: IMPACT OF APERIODICITY ON MODAL STABILITY AND ADVANCED DESIGNS TO IMPROVE THERMAL RESILIENCE




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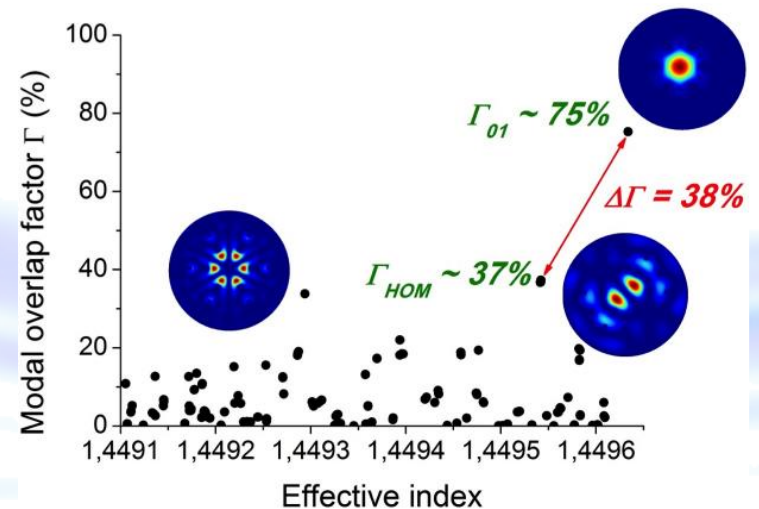
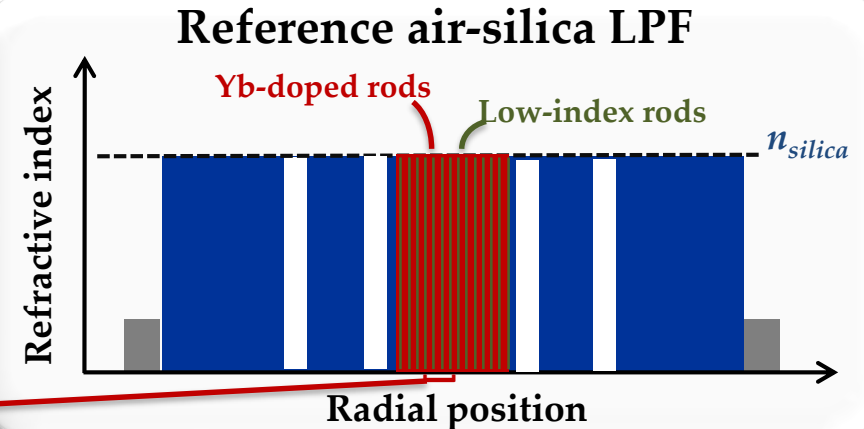
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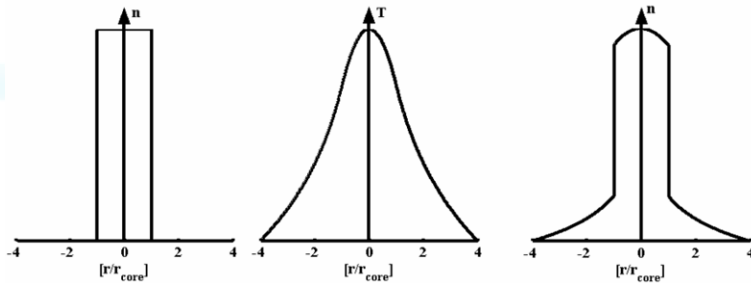


-  Gain material
-  Puresilica
-  Air Hde

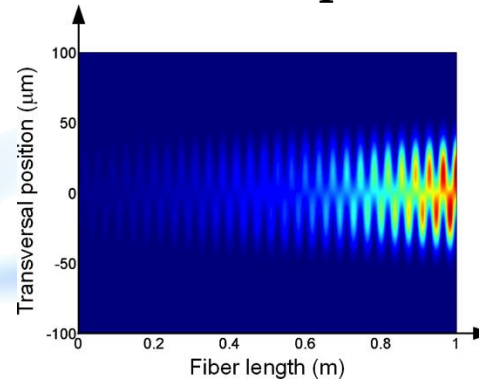


CRITERION $\Delta\Gamma$
MODAL DISCRIMINATION

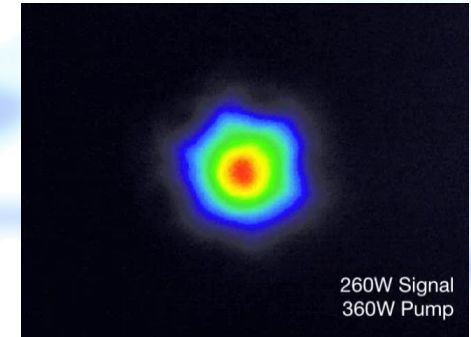
A thermal-induced process



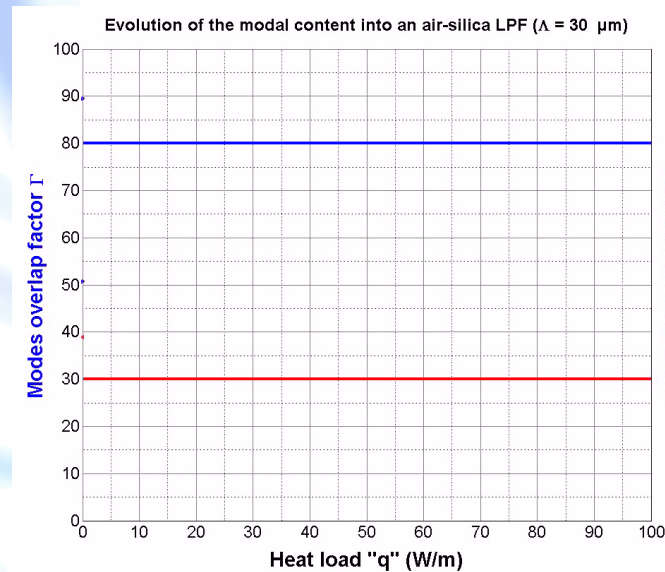
Hädrich et al., *Opt. Exp* 14(13) (2006)



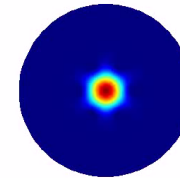
Jauregui et al., *Opt. Exp* 20(1) (2011)



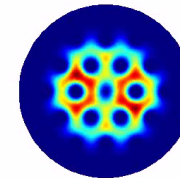
Eidam et al., *Opt. Exp* 19(4) (2011)



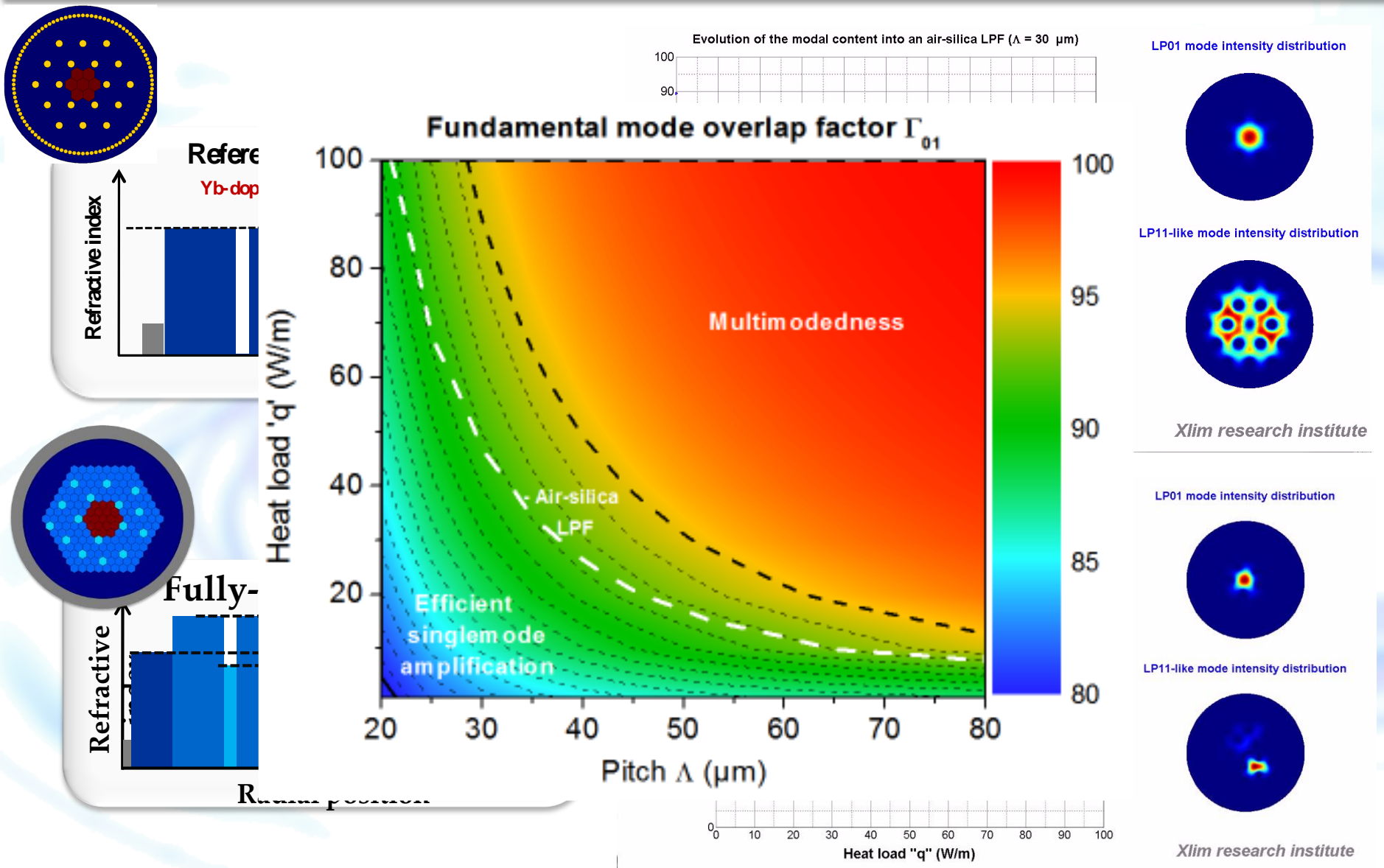
LP01 mode intensity distribution



LP11-like mode intensity distribution



Xlim research institute



REPUSIL manufacturing process

Powder sintering and vitrification



Schuster et al. (2014)

Assets

High optical quality
Production of large volume
Unique stack and draw

Cost effective fabrication

~~process~~

Control of the index-matching

Yb-doped material



Passively doped glass

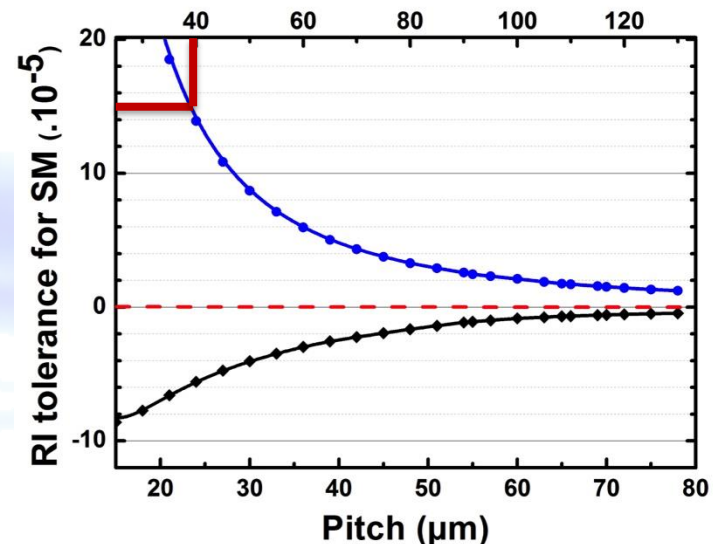


Device: Interfiber Analysis IFA-100

Accuracy: $\pm 1.10^{-4}$

Small index difference evidenced: $\sim 1.5.10^{-4}$

Gain region diameter (μm)



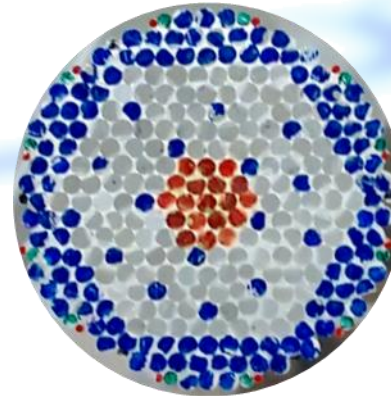
Yb-doped material



Passively doped glass



Stack



Core size

40 μ average

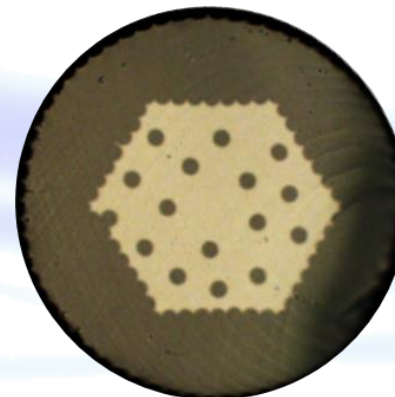
Air-clad diameter

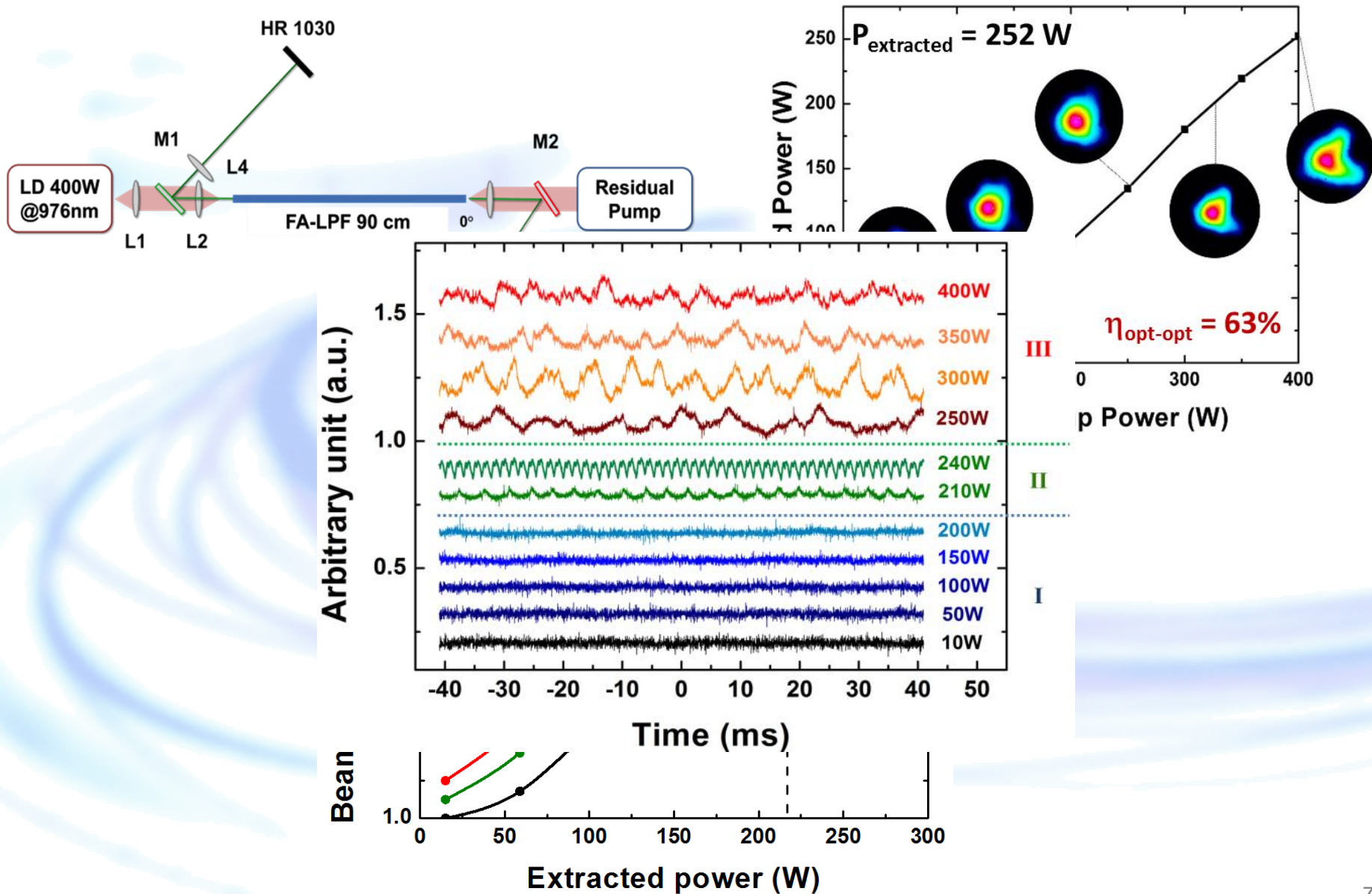
210 μ m – NA=0.45

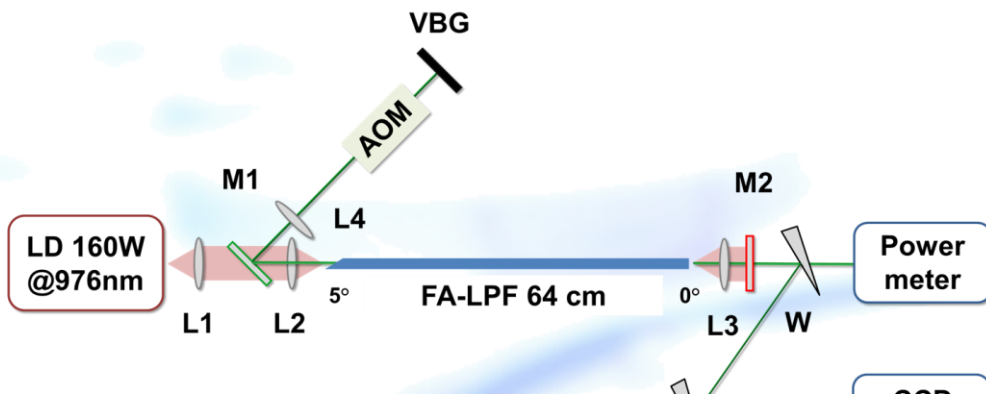
Rod-type outer diameter

1.2 mm

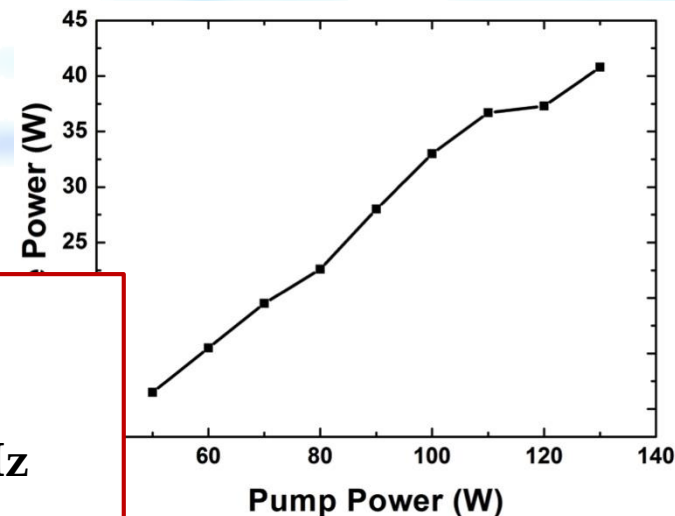
Yb-doped FA-LPF



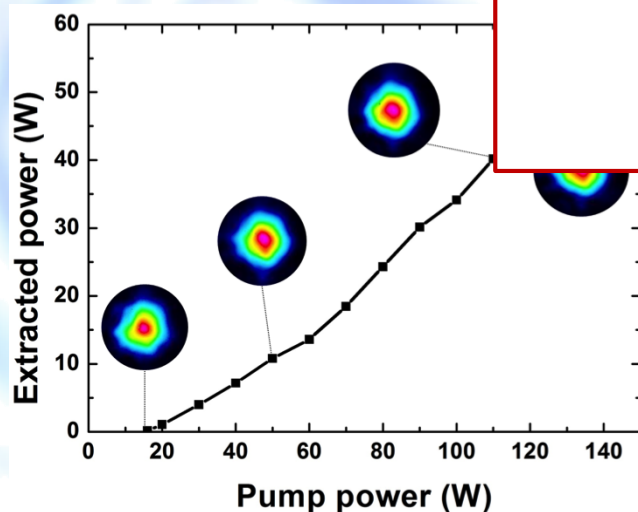




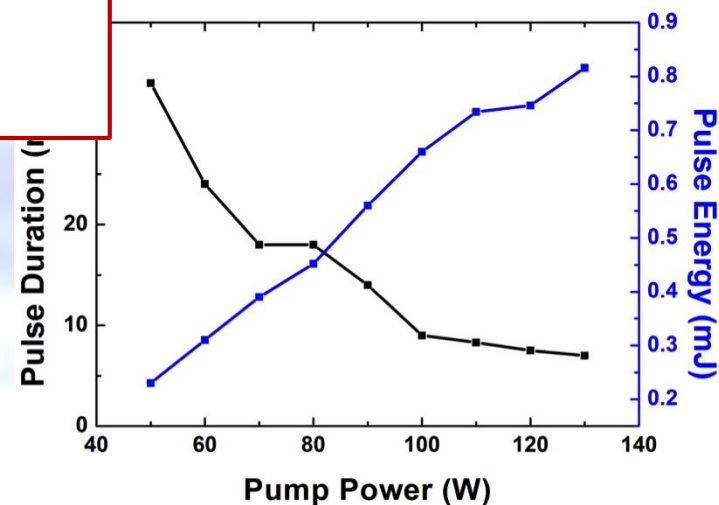
RR = 50 kHz
Endcap



RR = 100 kHz



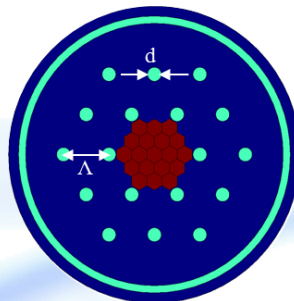
54W @100kHz
41W - 0.82 mJ @50kHz
 $M^2 \sim 1.4$



What about thermal pre-compensation at $2\mu\text{m}$?

FA-LPF vs LPF at $2\mu\text{m}$

LPF

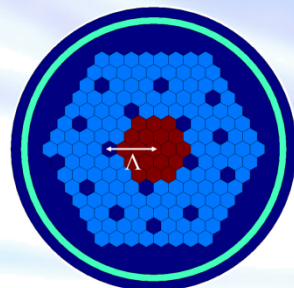


$$d/\Lambda = 0,3$$

$$\Lambda = 45\mu\text{m}$$

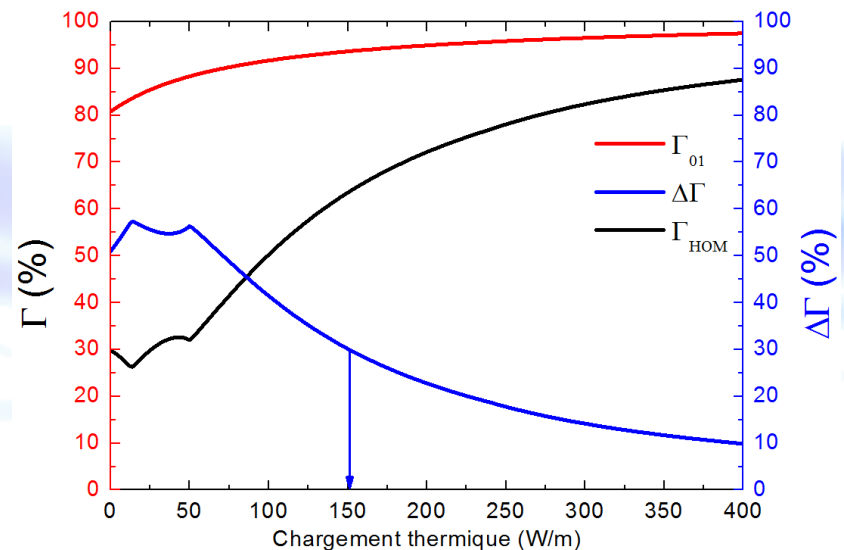
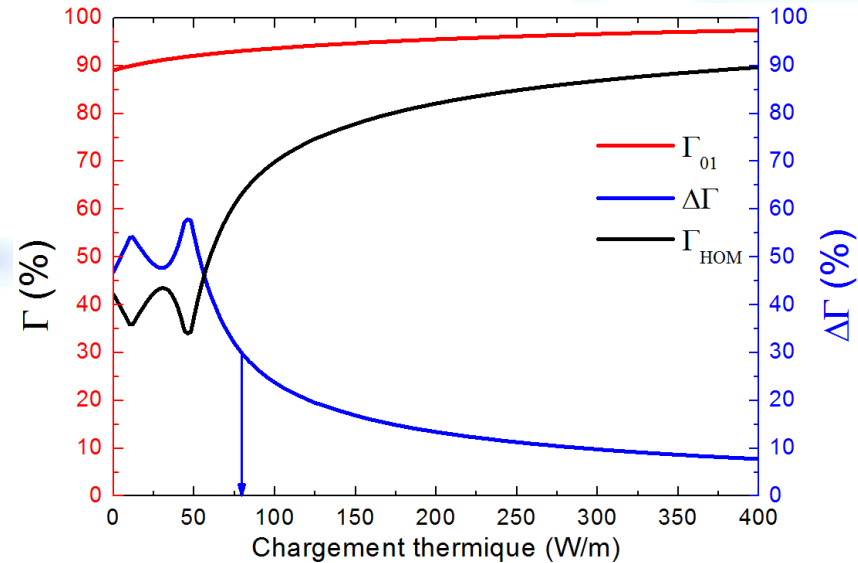
$$D_{\text{cœur}} = 76,5\mu\text{m}$$

FA-LPF



$$\Lambda = 45\mu\text{m}$$

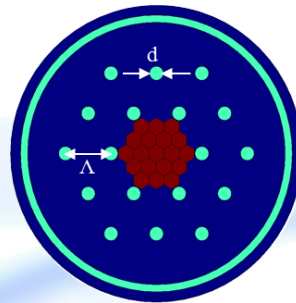
$$D_{\text{cœur}} = 76,5\mu\text{m}$$



What about thermal pre-compensation at $2\mu\text{m}$?

FA-LPF vs LPF at $2\mu\text{m}$

LPF

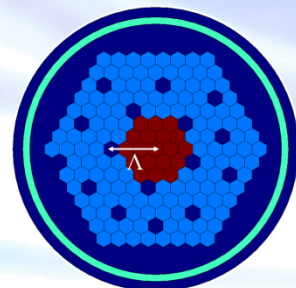


$$d/\Lambda = 0,3$$

$$\Lambda = 45\mu\text{m}$$

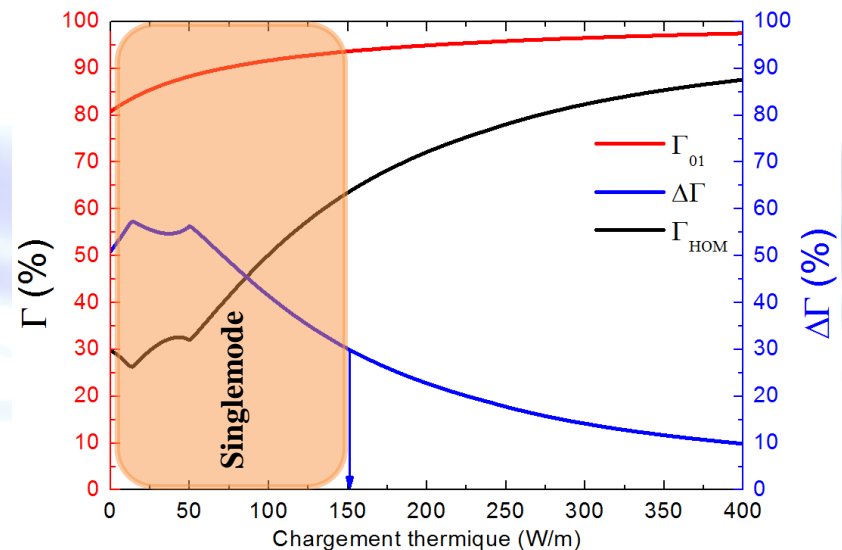
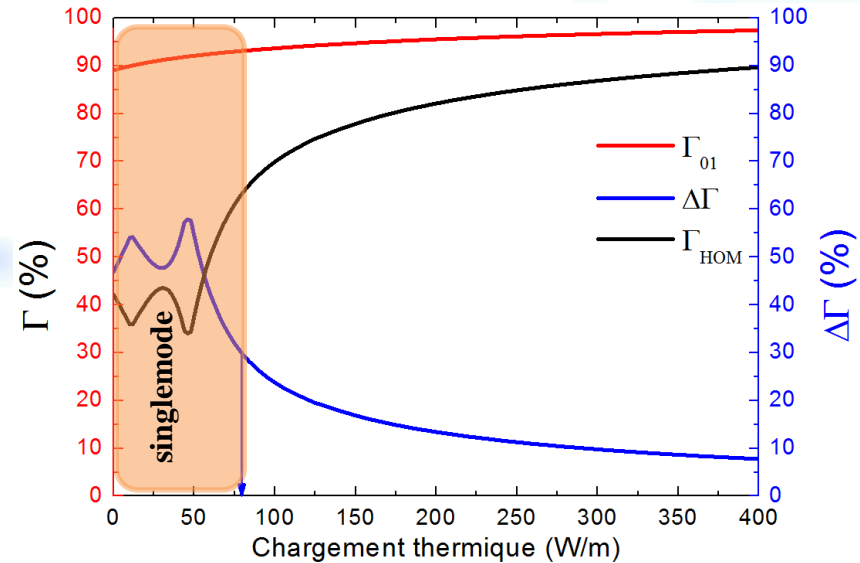
$$D_{\text{cœur}} = 76,5\mu\text{m}$$

FA-LPF

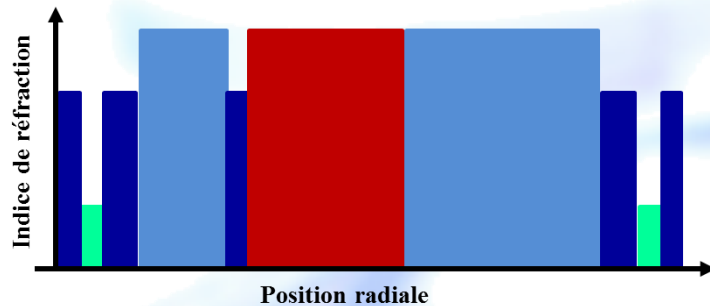


$$\Lambda = 45\mu\text{m}$$

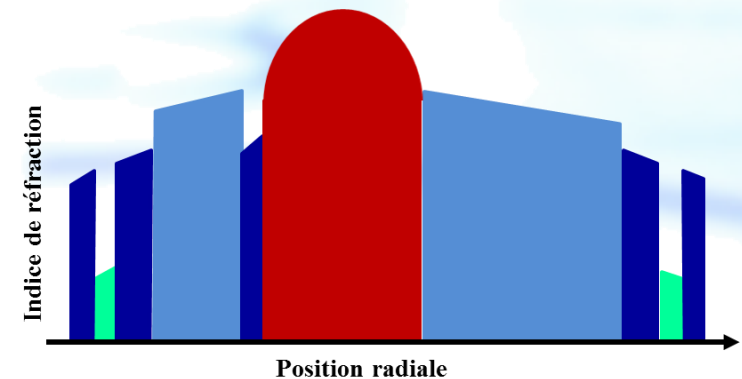
$$D_{\text{cœur}} = 76,5\mu\text{m}$$



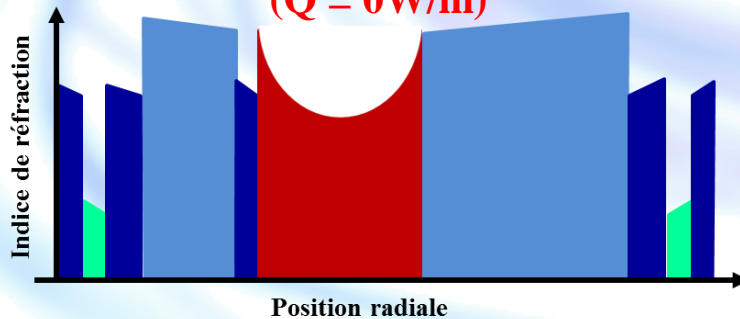
Transverse RI profile for cold fibre
($Q = 0\text{W/m}$)



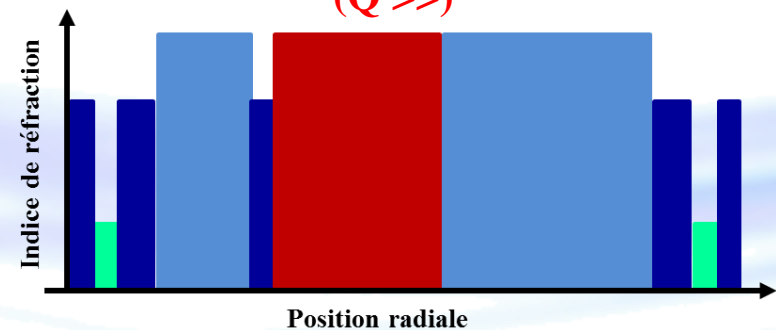
Transverse RI profile under severe heat load
($Q \gg$)



Intuitive pre compensated transverse RI profile for cold fibre
($Q = 0\text{W/m}$)



Expected transverse RI profile under severe heat load
($Q \gg$)



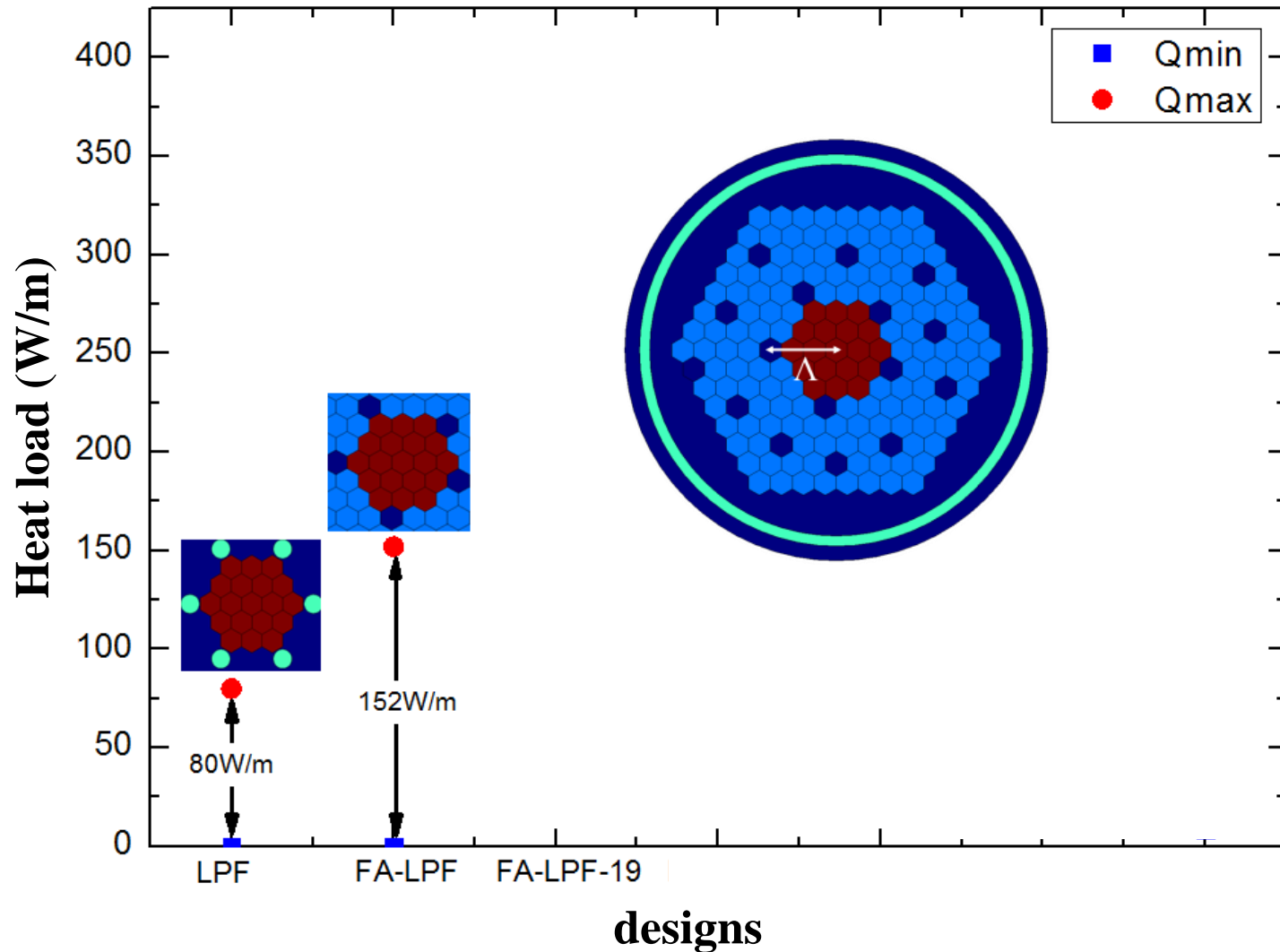
Two main problems: the fibre doesn't propagate FM when the fibre is cold

A 1×10^{-5} accuracy on RI value is required for each material whereas the current technology provide 1×10^{-4} to the very best

Limits are fixed
by

Qmin: $\Gamma_{01} = 80\%$

Qmax: $\Delta\Gamma = 30\%$

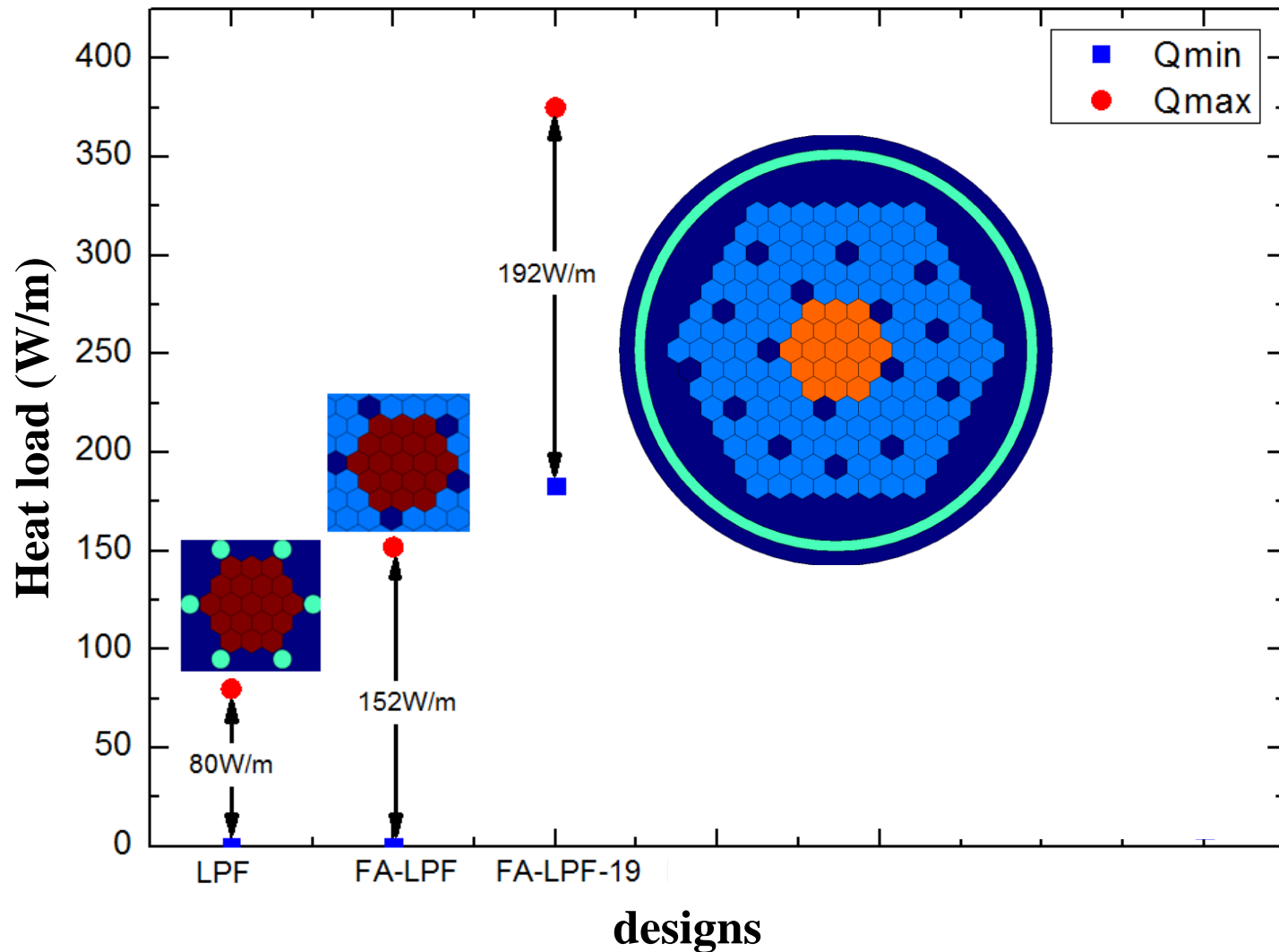


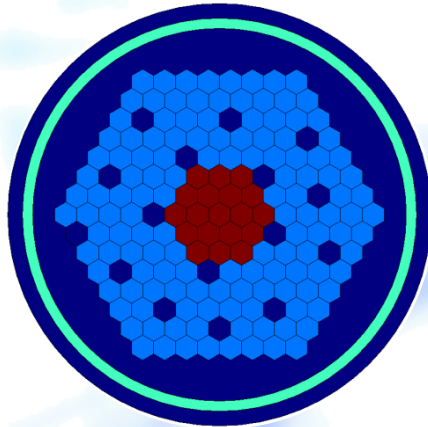
Amplitude of index depression 2×10^{-4}

Limits are fixed by

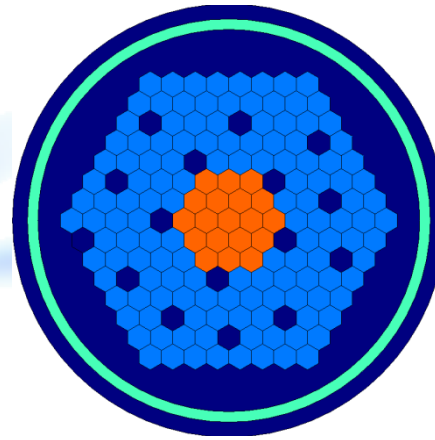
Qmin: $\Gamma_{01} = 80\%$

Qmax: $\Delta\Gamma = 30\%$

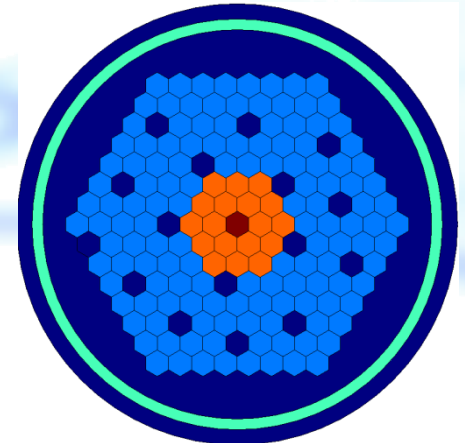




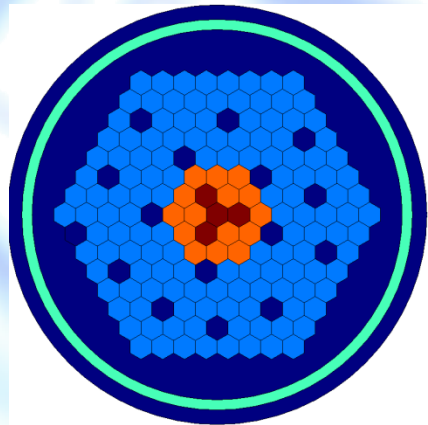
FA-LPF



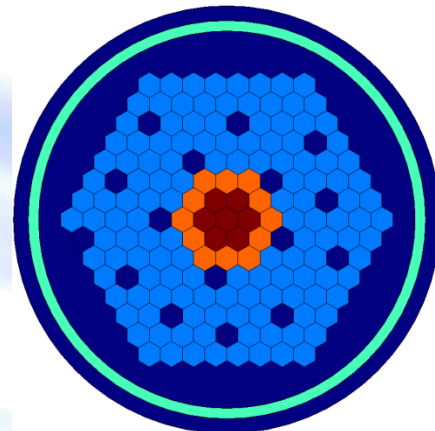
FA-LPF-19



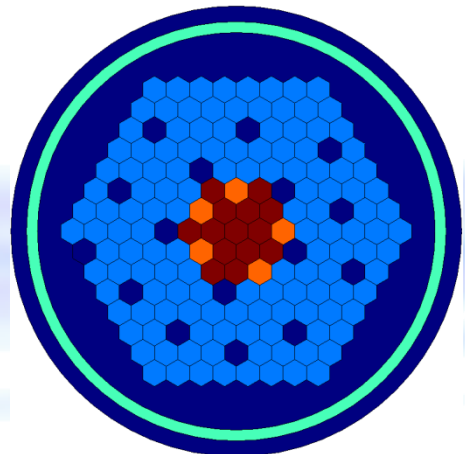
FA-LPF-18



FA-LPF-15



FA-LPF-12



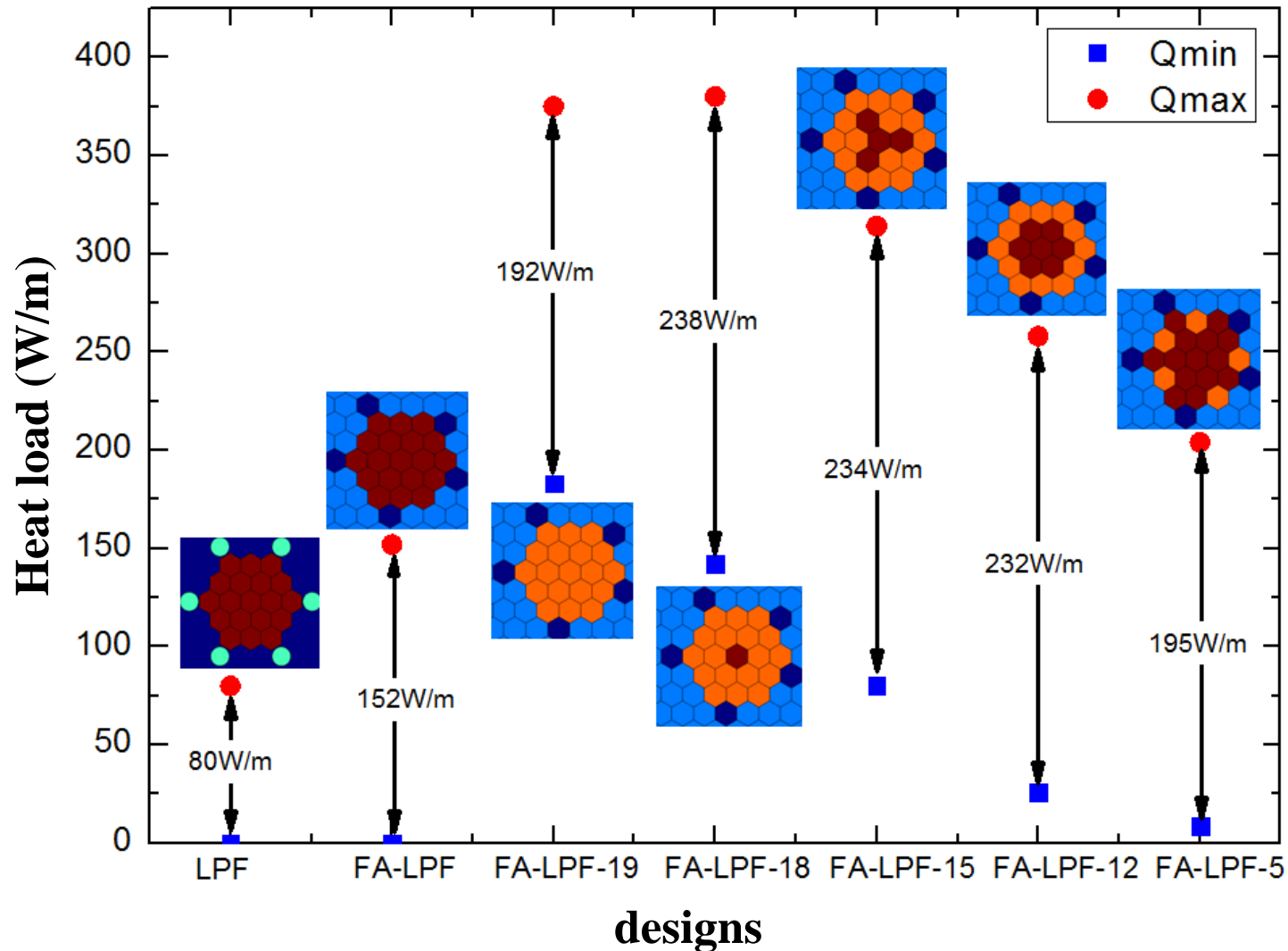
FA-LPF-5

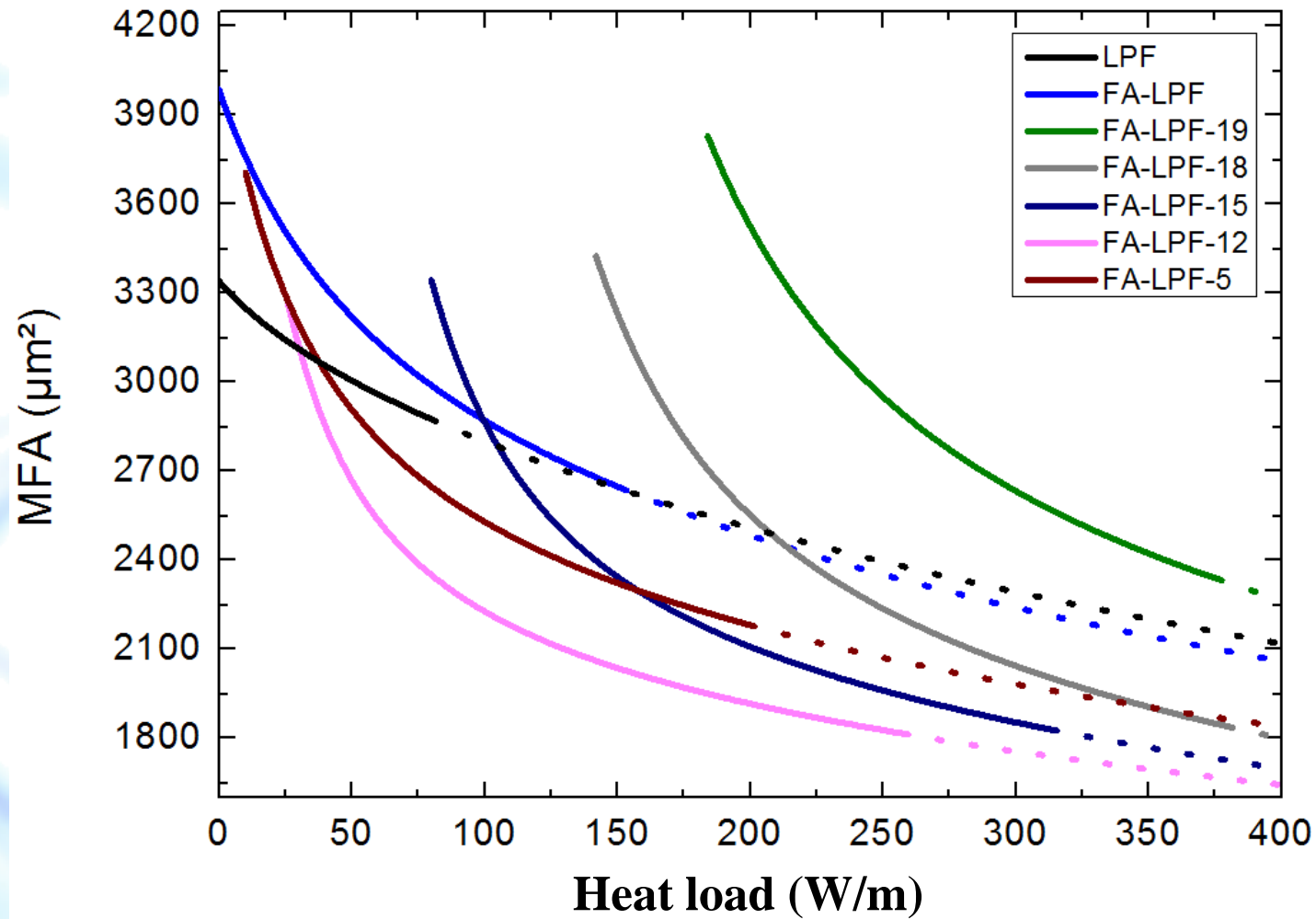
Dépression de 2×10^{-4}

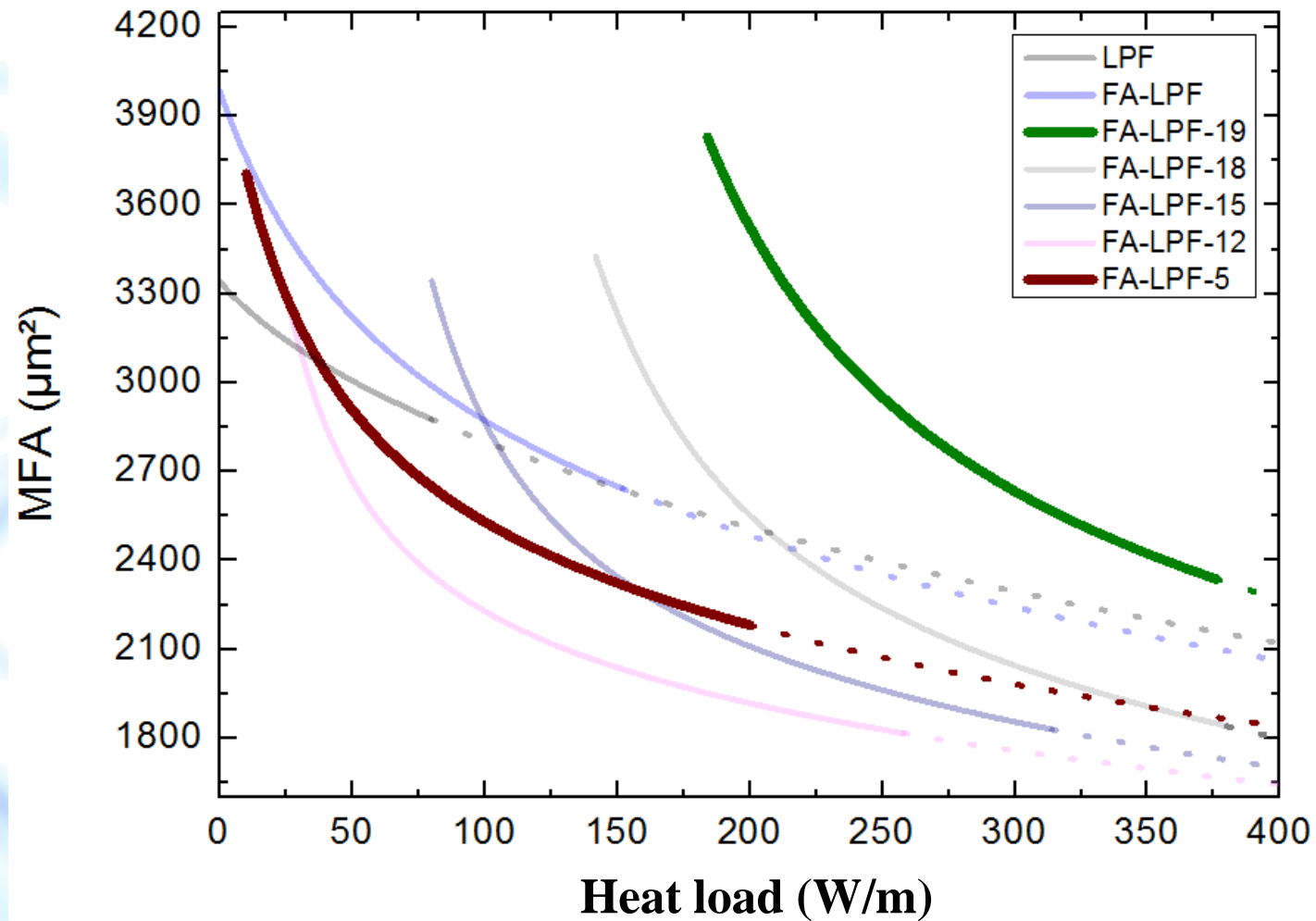
Limits are fixed
by

Qmin: $\Gamma_{01} = 80\%$

Qmax: $\Delta\Gamma = 30\%$







CONCLUSION

- ✓ FA-LPF design is intrinsically less sensitive to thermal loading
- ✓ First laser demonstration of non filamented Yb-core FA-LPF
- ✓ CW emission: 252W @ $M^2=1.4$ – $\eta_{\text{opt-opt}} = 63\%$ (MI threshold at 95W)
- ✓ Q-switch emission – 41W-0.82mJ @50kHz (MI threshold at 70W)
- ✓ Advanced but realistic designs can push away MI threshold provided material RI is accurately controlled

PROSPECTS

- ✓ Improve of the active/passive materials index
- ✓ Demonstrate Tm-doped FA-LPF and pre-compensated FA-LPF experimentally

THANK YOU FOR YOUR ATTENTION

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EOLITE LASERS IS GRATEFULLY ACKNOWLEDGE FOR ITS FINANCIAL SUPPORTS



RESULTS CAN IMMEDIATELY BE TRANSPOSED AT 2Mm, WOULD THERE BE AN ACTION IN THE FRAME OF COST MP1401?